

Manufacturing Feasibility Analysis and Load Carrying Capacity of Computer Numerical Control Cut Joints with Interlocking Assembly Feature

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The basic manufacturing feasibility and load carrying capacity of computer numerical control (CNC) were evaluated for router-cut joints. More precise and complex shaped geometry was cut on a CNC machine so that joint strength increased *via* providing a better self-locking system. Using the design for manufacture and assembly (DFMA) analysis, the raw material type and joint design were determined as the main drivers that have direct influence on the processing time and yield of the manufacturing process. Moreover, the bending moment capacity of the joints was determined in compression and tension testing and benchmarked those of rectangular mortise and tenon (RM&T) and dowel joints. The results showed that joints constructed of plywood performed better than those of medium-density fiberboard according to DFMA compliance score values. Moreover, the load capacity level of joints constructed of plywood provided stronger joints than MDF. In compression tests, CNC router-cut joints constructed of both plywood and MDF reached equal or higher strength relative to traditional joints. Furthermore, in tension tests, those of strength were lower compared to compression test results. The outcome of this study will contribute to the theoretical and practical knowledge of furniture joinery design.

Keywords: CNC router-cut joints; DFMA; Manufacturing feasibility; Static load test

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INTRODUCTION

The introduction of new technologies into an industry often results in production system changes. Although computer numerical controlled (CNC) technology was initially developed for metalworking, it has become popular for wood processing after the development of special software packages (Tannert *et al.* 2008). Increased flexibility, ability to cut complex geometric shapes, ability to produce complex three dimensional (3D) structures, a high level of machining accuracy, and the reduction of machine processing steps are some of the benefits of CNC technology (Tannert *et al.* 2008; Cheng *et al.* 2015).

Joints are arguably the most vital components in the furniture structure. Furniture failures more often occur due to loose or failed joints rather than fractured legs or rails (Eckelman 2003). Therefore, unreliable joints result in unreliable furniture (Smardzewski 2009). The strength capacity of joints could also rely on the self-locking mechanism, which provides better serviceability and durability performance (Snow *et al.* 2006; Tamke *et al.* 2008; Tannert *et al.* 2008; Simek and Vaclav 2010; Pang *et al.* 2011). Given the certain level of technological innovations, the nature of the CNC machines is highly suitable to produce 3D complex geometric shapes with increased manufacturing velocity, higher

accuracy, higher productivity rates, tight tolerances, and lower labor cost (Tannert *et al.* 2007, 2008; Tamke *et al.* 2008; Simek and Vaclav 2010). Although CNC manufacturing has many advantages, there are various drawbacks that occur during the manufacturing process due to certain machining conditions, namely processing time, thermal behavior, dynamic response, properties of material being processed (Akturk and Ilhan 2011; Cheng *et al.* 2015), and the inability to cut and pocket out sharp inner corners. In addition, there are some issues associated with the nature of wood and wood composites, such as grain orientation, corner splitting, or material burning (Tannert *et al.* 2008). However, the process itself, manufacturing quality, and variation within the process could be controlled if certain guidelines are followed (Kumar *et al.* 2009). In the literature, various types of CNC router-cut joints were studied for furniture and building constructions (Gros 2001; Davis 2006; Anastas 2007; Simek and Vaclav 2010). However, there is limited information that addresses the simultaneous definition of manufacturing feasibility and strength capacities of these joints.

Given ever-changing industry conditions driven by global trends (Stank *et al.* 2013), primary focus areas of this study are to determine the basic manufacturing feasibility and load carrying capacity of CNC router-cut joints, namely Dovetail (DT), Mickey Mouse Ear (MME), Blind Mickey Mouse Ear (B-MME), Snap (S), Blind Square Lock (BSL), Puzzle Lock (PL), and Blind Puzzle Lock (B-PL) joints. The manufacturing feasibility of each joint type has been evaluated for the determination of material yield, processing time, as well as design for manufacturing and assembly (DFMA) compliance score (Boothroyd 1994; Boothroyd *et al.* 2010). Within the scope of strength properties, samples of different joint types were tested for tension and compression. The results of strength tests were benchmarked with comparable traditional joint types- glued dowel, rectangular mortise, and tenon joints.

Determination of whether proposed joint designs could be manufactured has critical importance, because one of the most indispensable factors that add value to any research study is practicality and ability to solve industrial problems. This is the underlying reason why researchers have put extra effort into feasibility analysis. The purpose of a feasibility study is to evaluate and analyze the potential drawbacks and strengths of a proposed project to ease the decision-making process while selecting the CNC joint type. It is a useful tool to reach the optimal form of a production process in terms of manufacturing and cost efficiency (Whitten *et al.* 2001; Blanchard and Fabrycky 2010; Liu 2015). A feasibility analysis also helps to determine whether the project idea satisfies cost and technological constraints.

Current market trends and increased competitiveness within the industry has forced decision-makers to develop a way to optimize cost-effectiveness of the design process (Boothroyd 1994; Emmatty and Sarmah 2012). Formal developments in the field began towards the late 1970's, although the arrival of systems aiding with assembly time estimation took a couple more years until they were introduced in the early 1980's (Lefever and Wood 1996; Boothroyd *et al.* 2010; Arnette *et al.* 2014). Shortly after the introduction of these systems, design for manufacturing (DFM) and design for assembly (DFA) became popular because the concepts were designed to help with cost efficiency by eliminating waste through design and process improvements (Boothroyd 1994; Meeker and Rousmaniere 1996). Within the scope of this study, several quantitative analyses were conducted to test the efficiency of proposed joint types. Both DFM and DFA aim to reduce material and labor costs as a function of optimized product design and manufacturing

process planning. Therefore, they are often handled together as part of an integrated methodology called DFMA (Ashley 1995; Emmatty and Sarmah 2012; Barbosa and Carvalho 2013). Because the design process accounts for 70 to 80% of total manufacturing cost, it bears significant importance and deserves discussion (Meeker and Rousmaniere 1996; Bayoumi 2000).

While designing a new product, “the best part is no part” to reach the most efficient form of the process (Boothroyd *et al.* 2010; Barbosa and Carvalho 2013; Barbosa and Carvalho 2014). However, from the point of view of product strength design, the opposite would apply. Therefore, engineers in cooperation with process and product designers need to come up with the most practical and achievable design while keeping present technology and capital constraints in consideration. In any industry, minimizing the number of parts without compromising product performance is a good way to reduce inventory, which is the key transformation phase into a leaner enterprise (Demeter and Matyusz 2011; Hofer *et al.* 2012). This study also aims to ensure that proposed joint designs are compatible with the implementation of CNC-type automation.

The results of this study are expected to serve as a guideline for those interested in furniture, joinery design, understanding manufacturing feasibility, and strength properties of different joint types produced by CNC machinery.

EXPERIMENTAL

Materials and Specimen Construction

Medium-density fiberboard (MDF) (Menards, West Lafayette, IN, USA) and Baltic Birch plywood (DSA, Indianapolis, IN, USA) board, both widely used materials for furniture and cabinet manufacturing, were picked to prepare both CNC router-cut and traditional L-shape joint specimens. The mechanical properties of the MDF and plywood are shown in Table 1. Plain white oak (*Quercus alba*) dowels (Menards, West Lafayette, IN, USA) were used to construct the dowel joints. Polyvinyl acetate adhesive (PVA) (Franklin International, Columbus, IN, USA) at 40% solids content was used to assemble the joints.

Table 1. Selected Mechanical Properties of Wood Materials Used (Forest Products Laboratory 2010)

Material	Specific Gravity	Material Properties	
		Modulus of Elasticity (GPa)	Modulus of Rupture (MPa)
MDF	0.7 to 0.9	3.59	35.85
Plywood	0.4 to 0.6	6.96 to 8.55	33.72 to 42.61
White Oak	0.68	12.27	104.8

The CNC router-cut joints were designed and processed following the joint design process (Fig. 1) by using AutoCAD computer software (Autodesk, v. 2014, Mill Valley, CA, USA), MasterCAM computer software (CNC Software Inc., v. X8, Tolland, CT, USA), and a Thermwood Model 45 CNC router (Thermwood Cooperation, Dale, IN, USA).

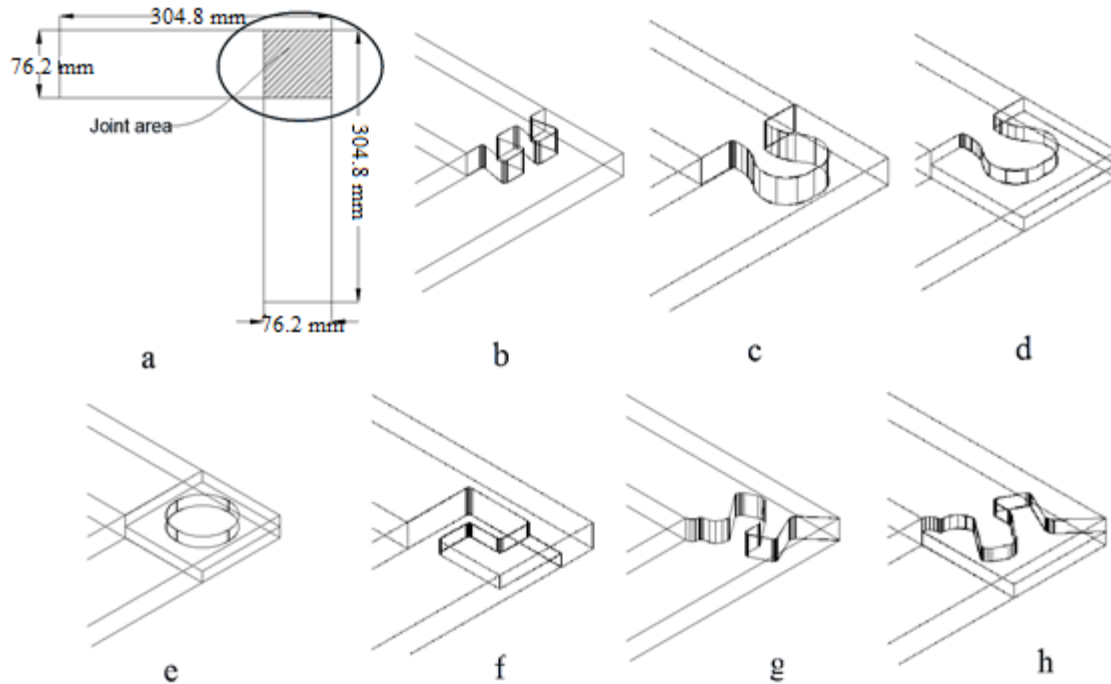


Fig. 1. CNC router-cut joints configuration: a: L-shaped joint, b: DT, c: MME, d: B-MME, e: S, f: SL, g: PL, and h: B-PL joints

In designing joints, the design existence in literature was used for DT, S, and SL were designed and developed by the authors, and the designs of PL, B-PL, MME, and B-MME were inspired by Gros (2001).

In CNC router-cutting, specimens were cut in two stages. The first stage utilized a 3/8 bit with cutting 17.75 mm and 6.35 mm in z-axes for counters and pockets, respectively. The second stage utilized a 3/16 bit with 1.25 mm and 3.15 mm in z-axes for counters and pockets, respectively. In total, 19 mm for counters and 9.5 mm for pockets were cut off. More detailed information on the cutting process and parameters is provided in Table 2. Utilizing a 3/8 bit ensured a faster and easier cutting procedure while the 3/16 bit was used to clean the edges and corners, with 0.001-mm tolerances.

Table 2. CNC Machinery Cutting Process

	Cutting Type	Material	3/8 bit ($r = 4.75$ mm)	3/16 bit ($r = 2.375$ mm)
Spindle Rate	-	-	18000 rpm	8149 rpm
Feed Rate			350 rpm	350 rpm
Deep Cut			6.35 mm	-
Depth	Counter	MDF	17.78 mm	1.27 mm
		Plywood	15.24 mm	3.05 mm
	Pocket	MDF	9.525 mm	9.525 mm
		Plywood	9.15 mm	9.15 mm

During the construction of mortise and tenon joints, tenons 31.25-mm-long by 50.8-mm-wide by 9.4-mm-thick were cut with a multi-chisel machine (Model 101L; Lorraine Machine, Inc., Greenville, SC, USA), as shown in Fig. 2. Matching mortises were cut by a router with 0.001-mm tolerances. The faces of the tenon and the walls of the mortise were coated with a 40% solid content PVA adhesive and the full length of the tenon was inserted into the mortise and clamped in place (Eckelman *et al.* 2016).

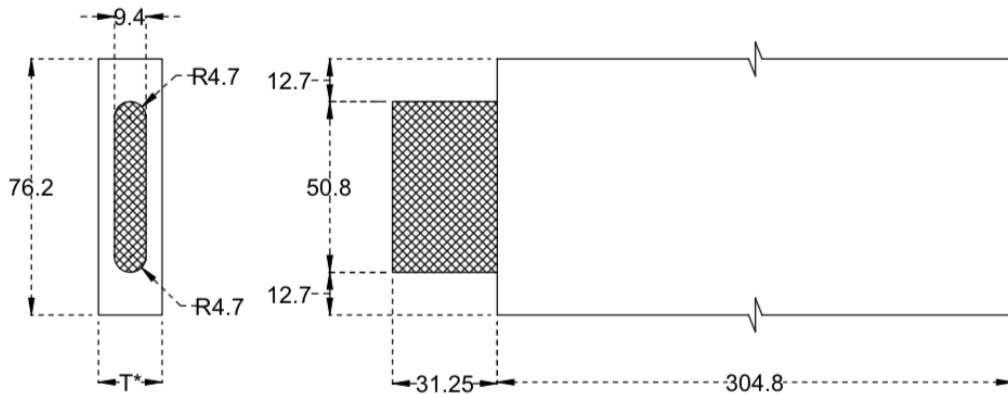


Fig. 2. Rectangular mortise and tenon joint configuration (mm, T* is 19 mm for MDF and 18 mm for plywood)

Plain white oak (*Q. alba*) dowels with 63.5 mm length and 9.4 mm diameter were used to construct the dowel joints. First, 31.25-mm deep dowel holes were drilled on the post and rails by using a multi-chisel machine, as shown in Fig. 3. The wall of drilled holes on posts and the half face of the dowels were generously coated with 40% solid content PVA adhesive and 31.25 mm length of the dowel was embedded on the post in the first stage. After at least 8 h of curing, the wall of drilled holes on the rails and the other half face of dowels embedded on posts were coated with adhesive and the post and rails were assembled (Eckelman *et al.* 2002). All specimens remained clamped for at least 24 h in an environment of 7% moisture content.

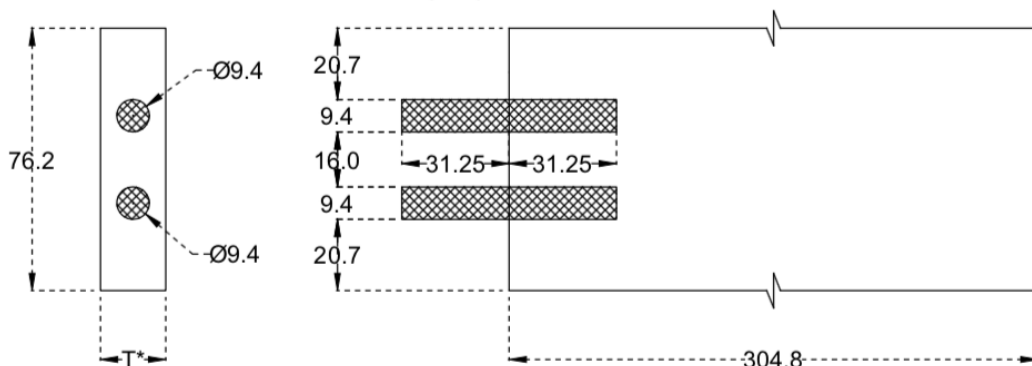


Fig. 3. Dowel joint configuration (mm, T* is 19 mm for MDF and 18 mm for plywood)

Methods

DFMA analysis

A key performance indicator (KPI), called DFMA compliance score was used to determine the DFMA performance of proposed joint types. Each joint type was evaluated

in terms of two main quantitative criteria, as they were commonly addressed in literature, namely insertion difficulty and handling difficulty (Boothroyd 2005; Boothroyd *et al.* 2010; Stienstra 2016). The insertion difficulty factor was calculated based on test results performed according to preset guidelines involving insertion time, alignment difficulty, secure fit rate after insertion, and required mechanical assistance during insertion, such as necessity to use a hammer to complete the installation process. The handling difficulty factor was determined as a combined function of handling time, weight, fragility, and flexibility (Kamrani and Nasr 2010). Various results from several analyses were put together on a Microsoft Excel (Microsoft Cooperation, v. Windows 10, Redmond, WA, USA) spreadsheet and were converted into a final grade on a scale from 1 to 10, resulting in a single DFMA performance indicator. The same analyses were independently conducted on plywood and MDF-based joints. However, other feasibility factors and strength properties that were discussed in this study also have crucial importance on general reliability decisions of joint types under investigation.

The guidelines for DFMA were defined under ten main titles in computer-aided manufacturing (Chang *et al.* 2006). During the entire design phase of proposed joint systems, considerable effort was put into ensuring that all the proposed joint designs conformed with commonly accepted DFMA principles. Therefore, this eliminated interfaces through use of self-locating features with the purpose of achieving a more optimized manufacturing process (Boothroyd 1994; Meeker and Rousmaniere 1996; Barbosa and Carvalho 2014). Final joint designs were determined at the end of detailed discussions and were picked among various alternative designs. It was expected that products with higher DFMA compliance rates would have lower manufacturing, assembly time, and cost. More reliable designs would lead to a high velocity production cycle-time from front-end to back-end throughout the production line.

Processing time and yield calculation

Manufacturing efficiency of CNC joints was determined by calculating the yield percentages for seven types of CNC router-cut joints. The CNC router processing times of the joints were determined to have better understanding of manufacturing feasibility for various joint types. For higher accuracy and reliability, processing times were obtained from MasterCAM 8 software, which was employed to create the design of each joint type, while the yield values were calculated by using the following formulas,

$$Y = 1 - \left(\frac{W_L}{W_M + W_L} \right) \quad (1)$$

$$Y_C = 1 - \left[\frac{(W_{L(Arm)} + W_{L(Post)})}{(W_{M(Arm)} + W_{L(Arm)}) + (W_{M(Post)} + W_{L(Post)})} \right] \quad (2)$$

where Y is the yield (%), W_L is the loss to cut (g), W_M is the mean processed material weight (g), Y_C is the combined yield (%), $W_{L(Arm)}$ and $W_{L(Post)}$ are the loss (g) to cut in arm and post components, respectively, and $W_{M(Arm)}$ and $W_{M(Post)}$ are the initial weight (g) of arm and post components, respectively.

The processing time per board area (PTBA) was used to determine the joint type with the fastest manufacturing time. Because the monetary value of time (Blank and Tarquin 2007) is essential in today's industrial world, faster manufacturing practices are desired and preferred. This parameter is designed to give the total board processing time for a particular joint type as if a complete board was cut to obtain the same type of joint component along the board area. Dimensions of the boards from which the joints were cut

out were 60" × 60" and 48" × 96" for plywood and MDF, respectively. This metric is appropriate to have a better understanding of manufacturing feasibility of joint types when large-scale production is considered within the scope of leaner manufacturing practices. It is essential to maximize yield and minimize any kind of waste to increase the velocity and efficiency of production systems, which directly contributes towards a pull production system.

Static loading test of joints

In this study, 90 specimens (70 CNC router-cut and 20 traditional joints) were evaluated to determine the compression and tension load capacity level of different types of L-shape joints cut out of MDF and plywood panels. All of the tests were performed on an MTS test machine (MTS Systems Corp., Eden Prairie, MN, USA) with 1000 N load capacity with a vertical loading rate of 12.7 mm/min (Eckelman *et al.* 2016).

The post of each specimen was mounted on the test jig with bolts. Load was applied on a moment arm of 254 mm from the face of the post, as seen in Fig. 4 (Erdil *et al.* 2005).

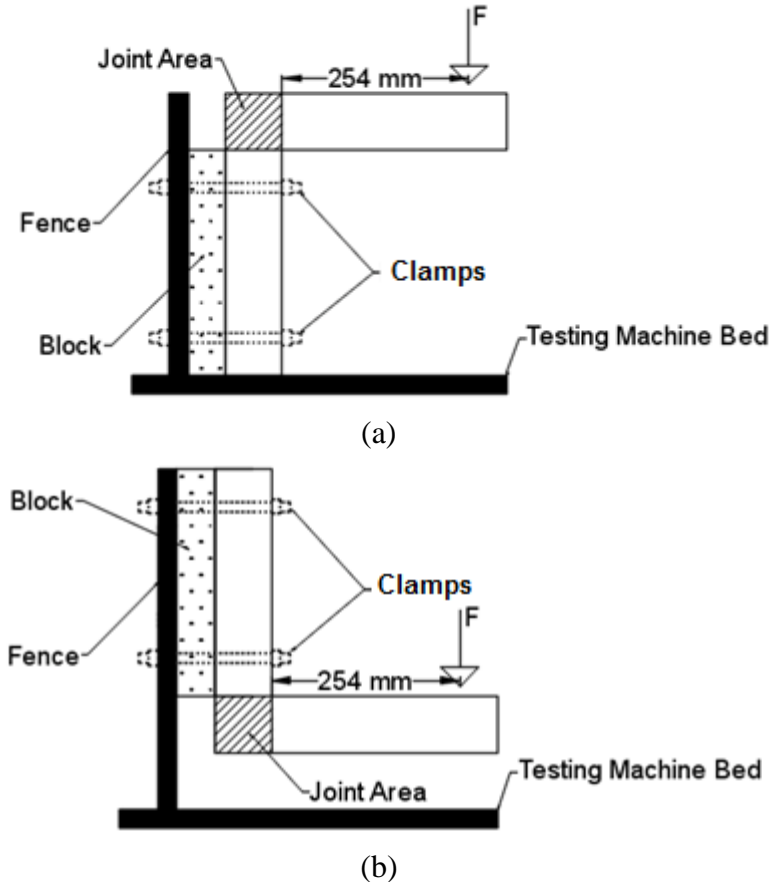


Fig. 4. Static test configuration: a: compression test and b: tension test

Bending moment capacity (M , in Nm) of joints was determined by multiplying the ultimate failure load (F , in N) with moment arm (L , in m):

$$M = F \times L \quad (3)$$

RESULTS AND DISCUSSION

The processing times per board area of the two components for each joint type were not combined. Such a combination would not have produced meaningful results in terms of having a complete understanding of manufacturing velocity and cost efficiency from the perspective of large-scale production. Therefore, PTBA analyses were run independently for each joint member based on the board type. Outcomes of PTBA analysis are expected to ensure that outcomes of this study will contribute to the furniture industry through practical findings.

The overall results of PTBA and total cutting time analysis did not yield drastically different results for joint members made of MDF or plywood, as can be seen in Fig. 5 and Table 3. Within the scope of total cutting time calculations, the CNC cut MDF joints had slightly better cutting velocity performance than their plywood counterparts. Furthermore, joints made of plywood had relatively higher velocity rates in terms of PTBA than those made of MDF, even though by the product structure, plywood is a denser and harder material than MDF.

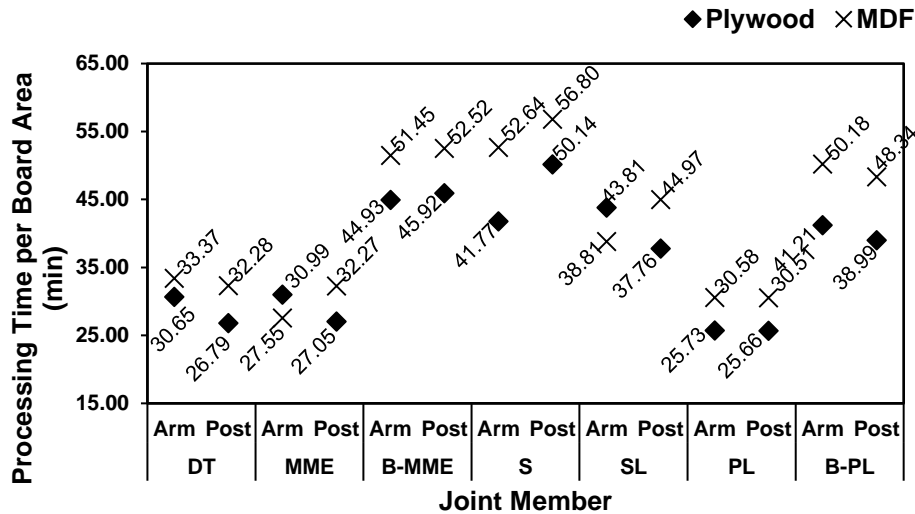


Fig. 5. Processing time per board area for joint members

Arm and post members of PL-type joints had the fastest processing time when compared to other joint types. They were followed by D and MME post members with values of 26.79 and 27.05 min, respectively. Although members of the PL-type joint yielded better PTBA results, low yield performance of the PL-type joint may hinder advantages gained in the means of PTBA. In contrast, PTBA values of DT and MME joint members were accompanied by the highest yield performance rates determined throughout the analysis. Therefore, manufacturing these two types of joints could be more favorable over other options if their strength properties can meet the requirements of certain furniture components. Strength properties of each type of joint was discussed in the related part of the study. Further feasibility interpretations could be made from the results shown in Tables 3 through 6. For instance, to manufacture DT-type joints, which require one MDF board for post and another board for arm members, the cutting process was calculated to take 57.44 min to complete the job, whereas S joint types required 91.91 min for the same

operation. This difference in time was approximately 60% slower under the same manufacturing conditions and for the same type of board.

Table 3. Total Cutting Time and Processing Time Per Board Area for Joint Members

Joint Type	Component	Time (s)				Time (min)
		Bit Type 3/8	Bit Type 3/16	Total Time (Member)	Total Time (Joint)	*Processing Time Per Board Area
Plywood						
DT	Arm	18.37	8.68	27.05	58.57	30.65
	Post	21.47	10.05	31.52		26.79
MME	Arm	18.60	8.74	27.34	59.16	30.99
	Post	21.71	10.11	31.82		27.05
B-MME	Arm	35.92	16.94	52.86	106.88	44.93
	Post	36.75	17.28	54.03		45.92
S	Arm	31.93	17.21	49.14	108.13	41.77
	Post	38.77	20.22	58.99		50.14
SL	Arm	26.24	12.42	38.66	83.08	43.81
	Post	30.11	14.31	44.42		37.76
PL	Arm	20.63	9.64	30.27	60.46	25.73
	Post	20.57	9.62	30.19		25.66
B-PL	Arm	32.23	16.25	48.48	94.35	41.21
	Post	30.26	15.61	45.87		38.99
MDF						
DT	Arm	18.79	6.88	25.67	55.47	33.37
	Post	21.89	7.91	29.80		32.28
MME	Arm	18.50	6.93	25.43	55.22	27.55
	Post	21.83	7.96	29.79		32.27
B-MME	Arm	27.47	20.02	47.49	95.97	51.45
	Post	28.75	19.73	48.48		52.52
S	Arm	27.27	21.32	48.59	101.02	52.64
	Post	28.64	23.79	52.43		56.80
SL	Arm	22.29	13.53	35.82	77.33	38.81
	Post	26.41	15.10	41.51		44.97
PL	Arm	20.63	7.60	28.23	56.39	30.58
	Post	20.57	7.59	28.16		30.51
B-PL	Arm	26.83	19.49	46.32	90.94	50.18
	Post	25.62	19.00	44.62		48.34
*PTBA represents the time (min) spent for manufacturing the same type of joint component along the one board area						

As shown in Table 4, the DFMA compliance score of CNC joints did not differ significantly between the two types of materials, namely plywood and MDF. Minor variations were observed for certain types of joints due to lower fragility grades recorded for some MDF joints. In terms of plywood-based joints, PL and B-PL had the highest DFMA fitting scores with grades of 9, which were followed by DT, MME, and B-MME joint types with grades of 8. The S-type joint system exhibited the worst DFMA fitting score of 6. In contrast, when DFMA analyses were run on MDF joints, the results were similar to those of their plywood counterparts. When compared to other types of MDF joints, B-PL and PL joint systems had the best DFMA fitting scores, as was the case for

plywood joint systems. Joints B-PL and PL had DFMA fitting scores of 9 while MME joints scored an 8.

The lowest DFMA performance grade was recorded for S-type joints with a score of 5, followed by SL joint systems that scored a 6. All of the designs, regardless of the raw material type, successfully satisfied the DFMA requirements for reduced number of parts, modular design, minimized assembly instructions, elimination of separate fasteners, and ease of fabrication. However, some joint types had lower performance results when it came to use of mechanical assistance to complete the insertion process. This is the main reason for the lower DFMA compliance indicator scores of certain types of joints. One explanation was that required mechanical assistance led to fragility problems in some joint types that also had negative impact on DFMA scores. When a cross-evaluation was made on yield and DFMA performance of joints for both material types, it was apparent that joint types with the best DFMA fitting scores were not accompanied with the highest combined average yield values. The results for the cross-evaluation can be seen in Table 4. Therefore, it may be more feasible and efficient to use DT and MME types of joints for large-scale production because they were the ones with the best yield performance and DFMA scores. However, this interpretation may differ based on the results of strength analysis and based on findings of future studies on the subject matter. The impact of strength analysis on such decisions is discussed in the following parts of the study.

As can be seen in Table 4 and Fig. 6, the overall yield performance results followed a similar pattern throughout the seven types of joints for two different material types, namely MDF and plywood. Yield analysis also revealed that MDF joints had relatively better yield performance values than those made of plywood. This may be due to the fact that plywood has a higher density value than MDF. Yield analyses were run based on two different material types used for specimens. Results of yield analyses conducted on joints revealed that DT and MME had the highest average yield values of 78.4% and 78.3%, respectively, when compared to those of the other 5 types of joints, whereas, PL had the lowest yield performance with 70.3%. The higher yield performance of DT and MME joint types were mainly influenced by high yield percentages of their post members. These two types of joints were followed by SL and B-PL type joints with yield values of 75.1% and 74.3%, respectively.

Joint members cut out of MDF boards had similar yield performance results with some minor variation in values of average yield and combined average yield performance when compared to plywood counterparts. Joints with the highest yield were DT and MME, at 80.3% and 77.1%, respectively. They were followed by SL, B-MME, and S with descending values of yield performance by 1% for all three types of joints. In terms of the lowest yield value, PL and B-PL completed the list at the bottom two rows with yield efficiency rates of 73.6% and 73.5%, respectively.

Statistical analysis run on SAS (SAS Institute, Cary, NC, USA) and Origin Pro Software (OriginLab Corporation, version 8.6, Northampton, MA USA) generated meaningful results when it comes to the assessment of correlation among dependent variables and factors being evaluated, as seen in Table 5. At the 0.05 significance level, two-way ANOVA results revealed that the population means of material type (MDF-plywood) were not significantly different from each other in terms of yield performance for proposed joint types, whereas the population mean of joint types were significantly different and had a P-value of 0.02143.

Table 4. Yield Performance and DFMA Compliance Rates of Joint Types

Joint Type	Part	Mean Weight (g)	Yield Calculations				DFMA Compliance Score*
			Average Loss to Cut (g)	Combined Loss to Cut (g)	Average Yield (%)	Combined Average Yield (%)	
PLYWOOD							
DT	Arm	331.62	105.11	173.95	75.9	78.4	8
	Post	292.40	68.83		80.9		
MME	Arm	318.06	118.67	177.22	72.8	78.3	8
	Post	302.69	58.54		83.8		
B-MME	Arm	302.62	134.11	251.59	69.3	71.2	8
	Post	319.26	117.47		73.1		
S	Arm	302.52	134.21	243.35	69.3	72.1	6
	Post	327.60	109.13		75.0		
SL	Arm	319.86	116.87	210.75	73.2	75.1	7
	Post	313.79	93.87		77.0		
PL	Arm	315.83	120.91	259.64	72.3	70.3	9
	Post	298.00	138.73		68.2		
B-PL	Arm	336.80	99.93	224.61	77.1	74.3	9
	Post	312.06	124.67		71.5		
MDF							
DT	Arm	294.28	82.23	157.46	78.2	80.3	7
	Post	356.37	75.23		82.6		
MME	Arm	307.44	103.67	191.71	74.8	77.1	8
	Post	343.56	88.05		79.6		
B-MME	Arm	335.88	95.73	213.92	77.8	75.2	7
	Post	313.41	118.20		72.6		
S	Arm	337.26	94.34	215.12	78.1	75.1	5
	Post	310.82	120.78		72.0		
SL	Arm	317.76	90.15	198.92	77.9	76.3	6
	Post	322.83	108.78		74.8		
PL	Arm	315.40	116.20	228.05	73.1	73.6	9
	Post	319.75	111.85		74.1		
B-PL	Arm	300.83	130.77	229.04	69.7	73.5	9
	Post	333.33	98.27		77.2		

*DFMA compliance score is a combined grade of Insertion Difficulty and Handling Difficulty performances of proposed joint types

It can be concluded that joint type had the largest impact on yield performance of the manufacturing process. In contrast, within the scope of processing time analysis, the population means of both material type and joint type were determined significantly different between the groups at a confidence level of 0.05, which meant both material type and joint type were important drivers of manufacturing velocity.

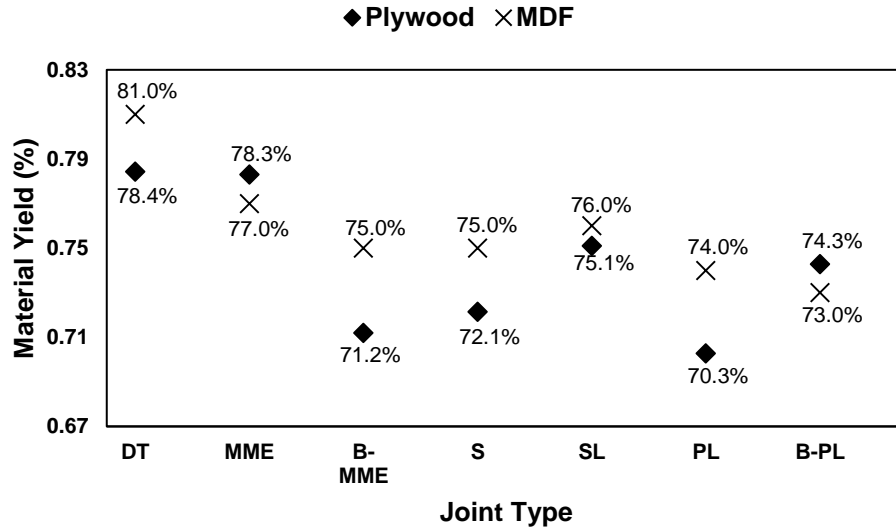


Fig. 6. Yield patterns of proposed joint types based on raw material type

Table 5. Two-Way ANOVA for Assessment of Differences Among Population Means

	DF	Sum of Squares	Mean Square	F Value	P Value
Material Type	1	9.04E-04	9.04E-04	3.7168	0.10214
Joint Type	6	0.00906	0.00151	6.2108	0.02143
Model	7	0.00996	0.00142	5.85451	0.02341
Error	6	0.00146	2.43E-04	--	--
Corrected Total	13	0.01142	--	--	--
ANOVA Analysis: Dependent Variable Yield, at 0.05 Confidence Level					
	DF	Sum of Squares	Mean Square	F Value	P Value
Joint Type	6	5452.79707	908.79951	234.413	7.62E-07
Material Type	1	104.72315	104.72315	27.0119	0.00202
Model	7	5557.52022	793.93146	204.784	1.04E-06
Error	6	23.2615	3.87692	--	--
Corrected Total	13	5580.78172	--	--	--
ANOVA Analysis: Dependent Variable Processing Time, at 0.05 Confidence Level					

Under current manufacturing conditions and stated technology limitations, it would be crucial to reach an optimal form of joint design for an increased yield and manufacturing velocity performance while material type decision would be considered as a critical factor only when it comes to processing time calculations.

The results of the static loading test of joint specimens are illustrated in Table 6, Fig. 7, and Fig. 8. In the compression static loading test of joints constructed of plywood, PL joints had the highest average bending moment capacity followed by the S joint, B-PL joint, B-MME joint, MME joint, and SL joint, whereas the DT joint had the lowest bending moment capacity. Overall, all CNC router-cut joints had higher average compression bending moment capacities than dowel joints. However, B-MME, S, PL, and B-PL had a higher bending moment capacity level and, MME and SL had roughly close bending moment capacities with RM&T, whereas only DT had lower bending moment capacity than RM&T.

Table 6. Average Bending Moment Capacity in Compression and Tension Test, and Glued Area of Joints

Joint Type	Plywood					MDF				
	Bending Moment (N.m)				Glued Area (cm ²)	Bending Moment (N.m)				Glued Area (cm ²)
	Compression		Tension			Compression		Tension		
DT	296.9	(1.6)	183.9	(9.9)	34.4	107.8	(7.1)	88.4	(6.0)	35.8
MME	363.4	(9.0)	99.0	(8.8)	31.5	81.6	(5.1)	83.8	(4.3)	32.8
B-MME	449.9	(4.0)	315.9	(5.7)	55.2	132.0	(8.5)	122.5	(4.4)	55.9
S	472.7	(15.1)	439.5	(11.6)	55.3	125.4	(5.7)	109.1	(8.7)	56.1
SL	355.7	(9.9)	142.1	(13.5)	51.9	137.6	(5.3)	42.7	(28.6)	53.2
PL	483.8	(6.3)	125.4	(5.7)	50.7	214.9	(4.1)	84.5	(8.0)	52.8
B-PL	457.6	(11.4)	132.9	(10.8)	53.7	133.1	(2.6)	79.8	(10.0)	54.6
Dowel	276.6	(18.5)	240.1	(14.7)	16.8	115.9	(17.0)	83.2	(12.7)	17.4
RM&T	370.6	(14.3)	327.7	(11.9)	41.1	125.4	(3.2)	103.0	(4.8)	41.7

*Values in parenthesis are the coefficient of variation (COV) of joints (in %)

As shown in Fig. 7, the compression test results of CNC router-cut joints constructed of plywood significantly outperformed those of MDF-based joints. Compression values of MDF-based joints varied from one design to another and performed at least 50% worse than plywood-based joints. For the comparison of the CNC router-cut joints to traditional joints, PL, SL, B-PL, and B-MME had a higher bending moment capacity level than both the RM&T and dowel, whereas DT and MME had lower bending moment capacities than RM&T and dowel joints. Moreover, the S joint had the same level of bending moment capacity with RM&T type joint.

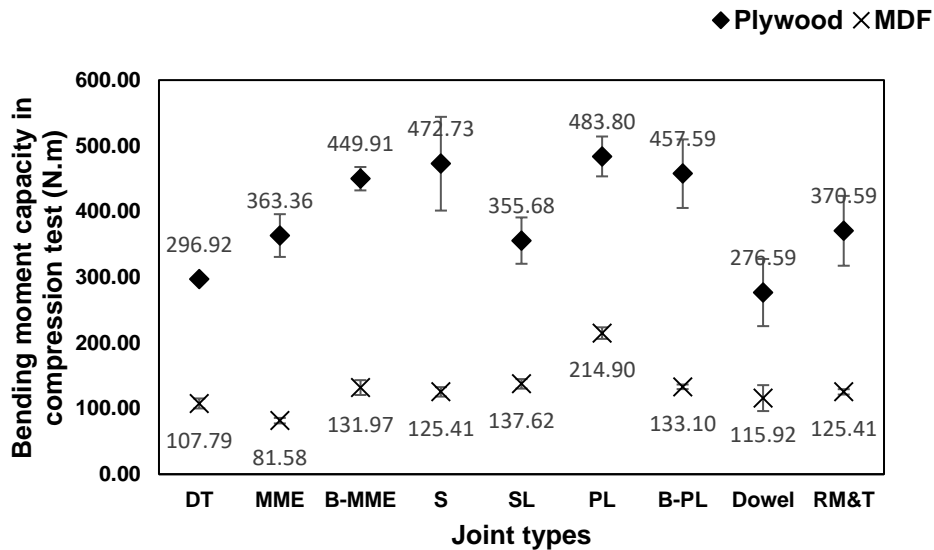


Fig. 7. Bending moment capacity of joints in compression test

In the tension static loading test of joints constructed of plywood (Fig. 8), the S joint had the highest bending moment capacity followed by B-MME, DT, SL, B-PL, PL, and MME joint. As shown in the same figure, the S joint and B-MME had a higher bending moment capacity level than that of dowel joints, whereas only the S joint had a higher bending moment capacity than the RM&T based on the results of compression tests. Although MME joints showed better performance in the compression test, they failed earlier because the size of neck in joints was not sufficient in tension.

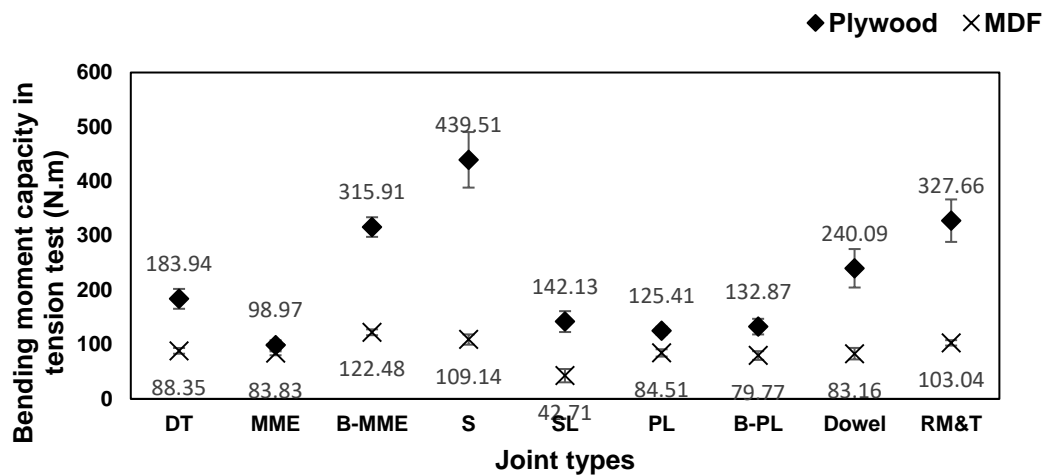


Fig. 8. Bending moment capacity of joints in tension test

Within the scope of the tension static loading test of joints constructed of MDF (Fig. 8), B-MME and S had higher bending moment capacities than the RM&T-type joint while B-PL and SL had a lower bending moment capacity level than traditional joints. The joint types that had better performance than the dowel joint type were B-MME, S, DT, PL, and MME.

Overall, the test results revealed that joints constructed of plywood had higher load capacity levels in both the compression and tension tests than those of MDF joints. Although joint geometry, adhesive type, manufacturing, and testing procedures were identical for both wood-based materials, the internal bonding strength of panels were different. The internal bonding strength of 38-mm-thick MDF was 0.51 ± 0.19 MPa (Rathke *et al.* 2012), while the internal bonding strength of the 9-mm-thick MDF and plywood was 0.57 MPa and 1.27 MPa, respectively (Suzuki and Miyagawa 2003). Therefore, failure of joints constructed of MDF occurred at lower load capacity levels than those of plywood. Furthermore, in both compression and tension test, the S joints made of plywood had higher standard deviation which could be due to S joints' weaker self-locking property compared to other joint types (Figs. 7 and 8). Underlying reason of such a wider variation in strength values of S joints could be due to increased prominence of certain failure types namely, shear on glueline and neck of snap. Furthermore, when results for its counterparts made of MDF are checked, this could also be interpreted as; S type joint design may not be the best option where plywood is preferred raw material for manufacturing. However, as given in Table 6, COV values in compression and tension tests for S type joints were 15.1% and 11.6%, respectively, and both were comparable to some of other joint types namely, B-PL, Dowel, and RM&T.

Both the plywood and MDF PL and B-PL joints had higher bending moment capacity levels in compression tests and lower bending moment capacity levels in tension tests than those of traditional joints. A self-locking characteristic provided the joints with more strength in the compression test. Even though they had more complex geometry, they could not provide higher strength than traditional joints due to the weakness of the self-locking characteristic in tension.

Table 7. Two-way ANOVA for Compression and Tension Test of Joints

	F-Value	P-Value	R ²
Compression Test			
Compression test	109.86	< 0.0001	0.963
Material type	1571.81	< 0.0001	0.810
Joint type	26.59	< 0.0001	0.110
Material*joint	10.39	< 0.0001	0.043
Tension Test			
Tension test	146.36	< 0.0001	0.971
Material type	1046.93	< 0.0001	0.409
Joint type	113.46	< 0.0001	0.355
Material*joint	66.7	< 0.0001	0.208

As can be seen in Table 7, a two-way ANOVA was conducted to evaluate the significance of material type and joint type on the strength properties of joints for bending moment capacity in compression and tension tests. Within the scope of the compression test, the material type, joint type, and combined effect of both the material type and joint type were determined significant at the 0.05 significance level. Variation in joint strength can be explained by the material type, joint type, and interaction of material, respectively by, 81%, 11%, and 4.3%. In tension tests, the material type, joint type, and material were significant at the 0.05 significance level. Moreover, the material type, joint type, and interaction of the material and joint type were responsible for 40.9%, 35.5%, and 20.8% of variation in tension test results of joints, respectively.

Bonferroni groupings were run to examine the differences among the proposed joint types in terms of variation in strength properties as shown in Tables 8 and 9. Based on the grouping results, the mean of the joint strength represented with same letter were not significantly different from each other at a 0.05 significance level. In the compression test, for joints constructed of plywood the PL and S joints were significantly different from the RM&T joint while the PL, S, and BPL joints were significantly different from the dowel joint. For the tension testing, only the B-MME joint was not significantly different from the RM&T joint while only DT was not significantly different from the dowel joint. For the joints constructed of MDF in compression testing, the PL and MME joints were significantly different from the RM&T joints whereas the PL, SL, and MME joints were significantly different from the dowel joint. For those of the tension tests, the S and DT joints were not significantly different from the RM&T as the B-MME, S, and SL joints were significantly different from the dowel joint.

Table 8. Bonferroni Grouping Test for Joints Constructed of Plywood

Compression Test					Tension Test						
Bon Grouping			Mean	N	Joint	Bon Grouping			Mean	N	Joint
	A		483.8	5	PL		A	439.5	5	S	
	A		472.7	5	S		B	327.7	5	RM&T	
B	A		457.6	5	B-PL		B	315.9	5	B-MME	
B	A	C	449.9	5	B-MME		C	240.1	5	Dowel	
B	D	C	370.6	5	RM&T	D	C	183.9	5	DT	
B	D	C	363.4	5	MME	D	E	142.1	5	SL	
	D	C	355.7	5	SL	D	E	132.9	5	B-PL	
	D		296.9	5	DT	D	E	125.4	5	PL	
	D		276.6	5	Dowel		E	99.0	5	MME	

Table 9. Bonferroni Grouping Test for Joints Constructed of MDF

Compression Test					Tension Test						
Bon Grouping			Mean	N	Joint	Bon Grouping			Mean	N	Joint
	A		214.9	5	PL		A	122.5	5	B-MME	
	B		137.6	5	SL	B	A	109.1	5	S	
C	B		133.1	5	B-PL	B	C	103.0	5	RM&T	
C	B		132.0	5	B-MME	D	C	88.4	5	DT	
C	B	D	125.4	5	S	D		84.5	5	PL	
C	B	D	125.4	5	RM&T	D		83.8	5	MME	
C		D	115.9	5	Dowel	D		83.2	5	Dowel	
		D	107.8	5	DT	D		79.8	5	B-PL	
	E		81.6	5	MME		E	42.7	5	SL	

Another two-way ANOVA was conducted to evaluate the relationship between CNC router-cut joint strength and glue area (or joint interaction area). The results of this analysis indicated that the relationship between the joint strength and glue area was significant at a 0.05 confidence level, as shown in Table 10.

Table 10. Two-way ANOVA Analysis for Strength and Glue Area Relationship for CNC Router-cut Joints

Material Type	Type of Test	F-value	P-value	R ²
Plywood	Compression	15.96	< 0.0001	0.773
	Tension	138.79	< 0.0001	0.967
MDF	Compression	148.02	< 0.0001	0.969
	Tension	146.36	< 0.0001	0.971

Future Work

Providing a better self-locking characteristic for CNC Router-cut joints in tension tests could be concern for future study. Moreover, conducting future DFX studies that address different aspects of engineering design and measure the impact of different types of glues on the strength properties of proposed joint types would contribute greatly to the literature of wooden furniture joints.

CONCLUSIONS

This paper aimed to determine the basic manufacturing feasibility and load carrying capacity of L-shape CNC router-cut joints. Assembly and manufacturing feasibility of joint designs was examined through design for manufacture and assembly (DFMA) analysis, while the load capacity tests evaluated whether the proposed joint types comply with certain strength requirements critical for the furniture industry. Within the scope of this study, theoretical arguments were supported with practical applications and statistical analysis to provide readers with a full understanding of the design and manufacturing processes related to certain joint types, as well as to document strength properties of proposed joint types under certain conditions. Research questions related to feasibility and strength design concepts were answered through a systematic methodology and valuable results were obtained.

1. Through DFMA studies, it was found that most of the proposed joint types could be manufactured in an industrial setting. However, it was also found that some proposed joint types could generate less efficient performance results depending on raw material type and joint design, correspondingly; cutting time of joints made of medium density fiberboard (MDF) were 3.6% to 10.2% less compared to those of plywood whereas they provided 1.2% to 5.1% higher yield excluding Mickey Mouse Ear (MME) (-1.7%) and Blind Puzzle Lock (B-PL) (-1.8%) joints. Moreover, average DFMA compliance scores were 7.85 and 7.28 out of 10 for joints made of plywood and MDF, respectively.
2. Joints made of plywood had higher strength properties compared to those of MDF owing to its higher internal bonding strength and mechanical properties. Therefore, joints made of plywood are recommended to utilize in furniture structure where higher strength values are required; in epitome, frames of sofas, *etc.* On the other hand, joints made of MDF could be used in furniture or cabinet structure where light-duty load and light structure are required such as cabinet doors.
3. Bending moment capacity in compression test results for joints made of both plywood and MDF were higher than those of tension with exceptions for Blind Mickey Mouse Ear (B-MME) and snap (S) joints, for which compression and tension strength values were reasonably close to each other. Joint types lacking self-locking system provided less strength in tension. Therefore, these type joints should not be used in furniture structure where imposed strength exceeds their strength whenever the joint are subject to tension load.
4. A load capacity analysis revealed that CNC router-cut joints made of both plywood and MDF provided better or reasonably close strength values when compared to those of traditional joints. This was, especially in compression tests, due to complex joint geometry. Therefore, it could be preferred to utilize CNC-cut router joints in furniture

structure where compression load is primary concern. On the other hand, for the cases where furniture joints are to resist tension load, B-MME and S type joints made of plywood should be used because they were able to provide higher strength values compared to traditional joints.

5. Reduced manufacturing time and increased yield performance could help companies save money if DFMA principles are methodically implemented. In conclusion, although joints made of MDF provided faster cutting time and higher yield compared to those of plywood, they were not as efficient as their counterparts made of plywood in terms of DFMA compliance score and strength in both compression and tension. Therefore, requirements of different furniture structures should be well considered before reaching to a final decision on which joint and raw material type to utilize.

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